

Deposition of hard highly transparent abrasion-resistant DLC on glass

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Content of presentation

- Carbon sputtering, HIPIMS discharge and effect of positive voltage reversal
- Deposition of carbon from a dual rotatable magnetron
- Importance of electron extraction, magnetic guidance
- Hard coatings on insulating substrates: DLC on glass with Hipims and Switching Power

Introduction – Carbon by magnetron sputtering

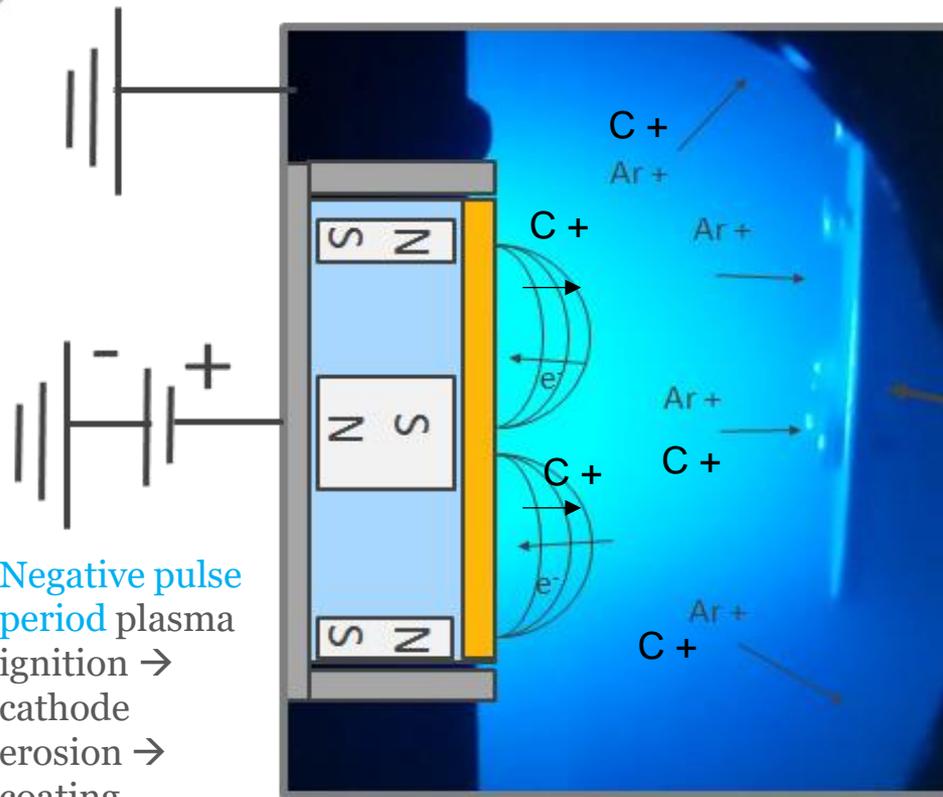
- The sputter deposition of carbon is characterised by a very low sputter rate.
- The two most common allotropic forms of carbon (diamond-like and graphitic) can be deposited, depending of several factors.
- The deposition of diamond-like carbon (DLC) coatings requires some levels of bombardment (ions, electrons) on the substrates. Harder DLC typically requires higher ion bombardment.

Introduction – Positive bombardment for DLC coatings

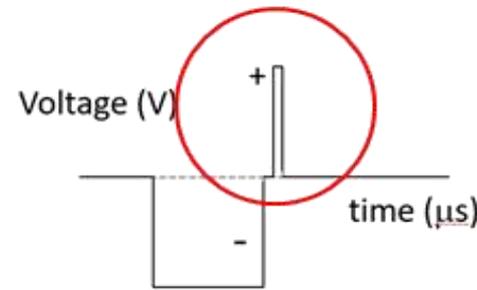
- DLC coatings can be produced via PACVD methods from precursors, with the use of ion sources.
- In magnetron sputtering from carbon targets, positive ion bombardment can be ensured by magnetic design (unbalanced) or external elements (e.g. hot filaments, independent ion sources).
- Hard coatings are favoured by the possibility of negatively biasing the substrate
- Ion exposure can be also guaranteed by a control of the plasma discharge.

Positive Voltage Reversal Effect

Below is the schematic of the sputter target voltage with a short time +ve pulse (reversed phase) in order to bombard the growing carbon coating

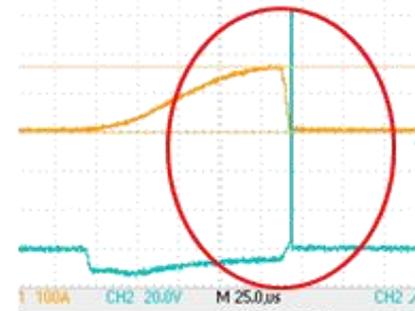


Negative pulse period plasma ignition → cathode erosion → coating deposition

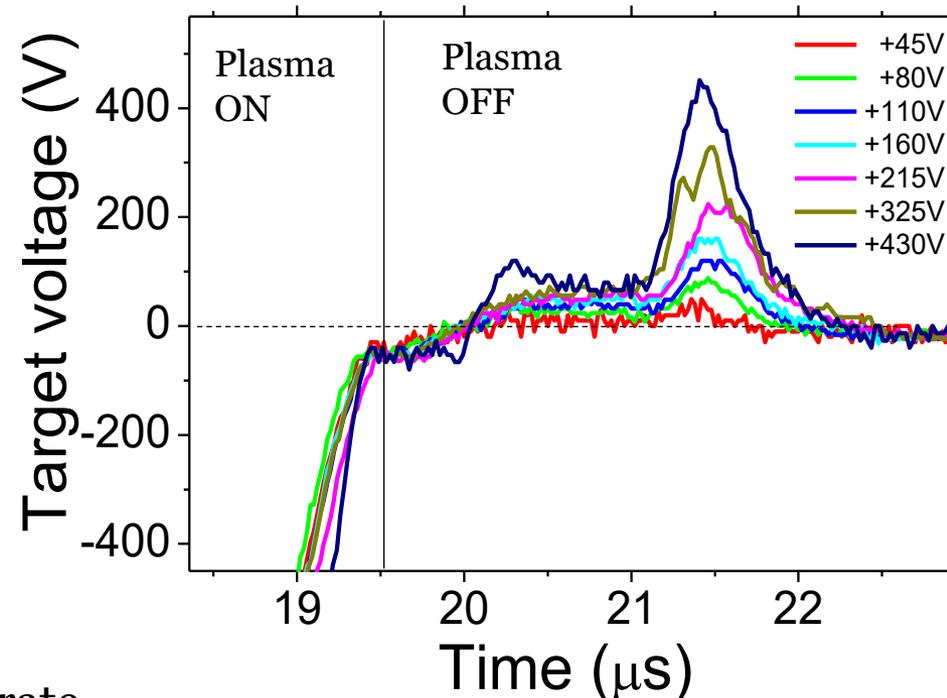
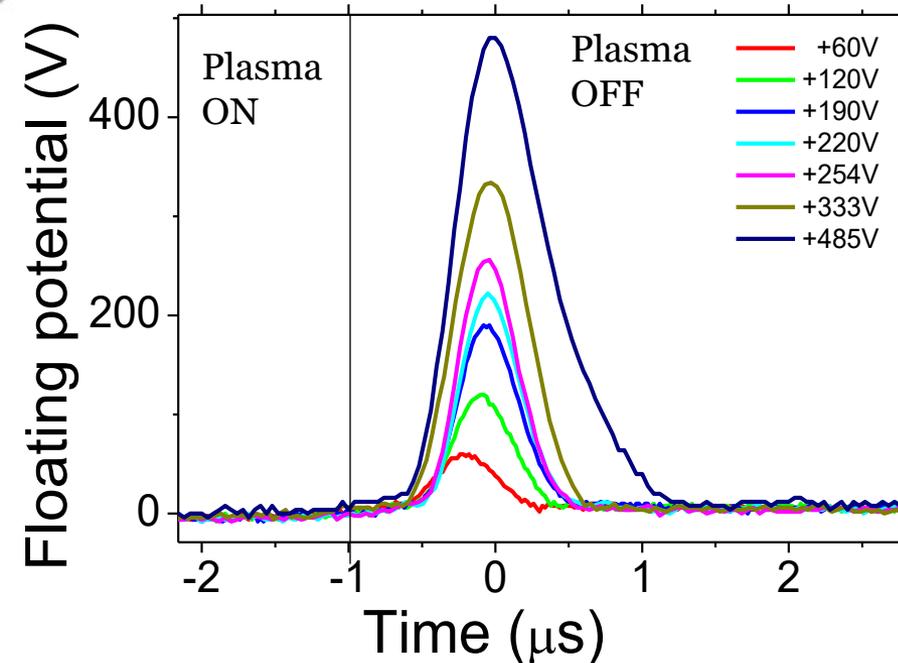


Positive pulse period plasma extinguish → fast plasma potential raise → positive ion acceleration towards grounded substrates

Floated substrate



The power supply applies a negative bias to the target to sputter the carbon followed by a positive bias in order to bombard the carbon layer with energetic species and ions



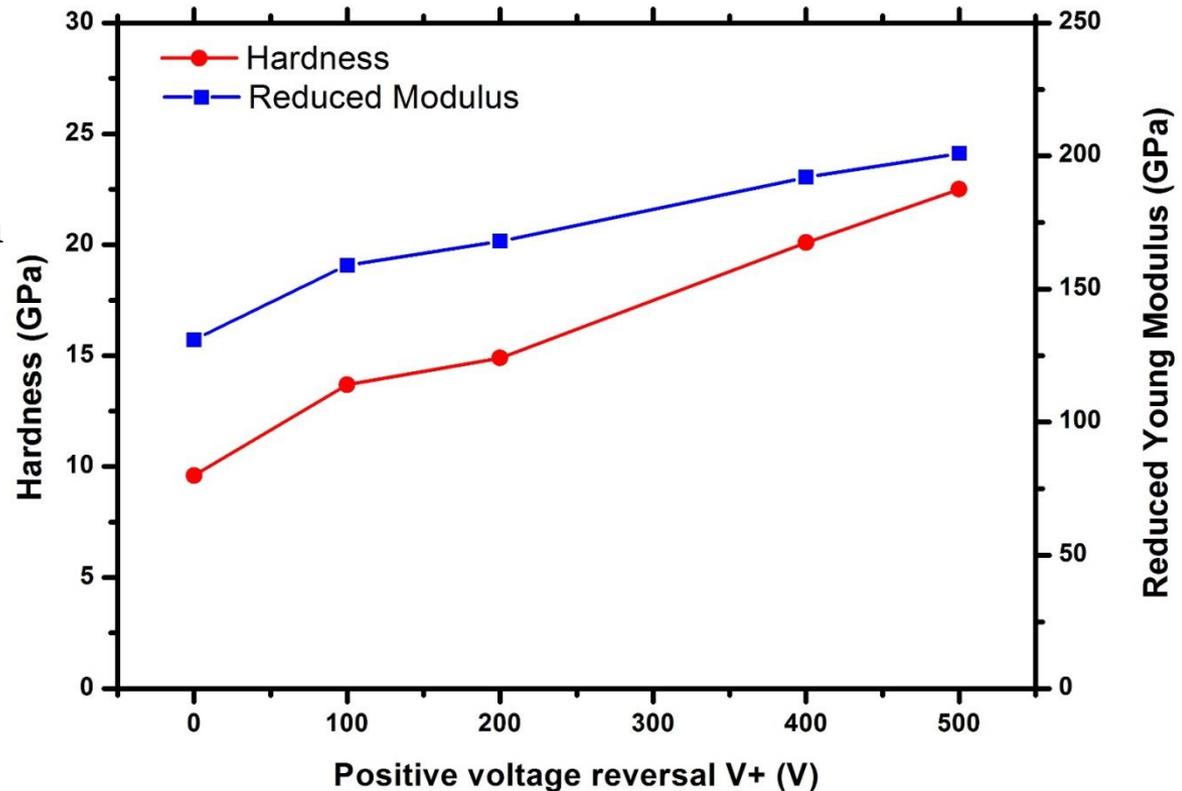
The above floating potential is the substrate potential and assumes about the same level as the target positive reversal voltage

Effect of positive pulse reversal on the hardness of sputtered carbon on glass

The hard carbon deposition method uses a positive pulse reversal via the HipV⁺ power supply combined with electron guiding within the sputter chamber - patent pending

The higher the positive pulse, the more the bombardment and the harder the carbon layer

This 'smart' ion assistance does not require additional sources

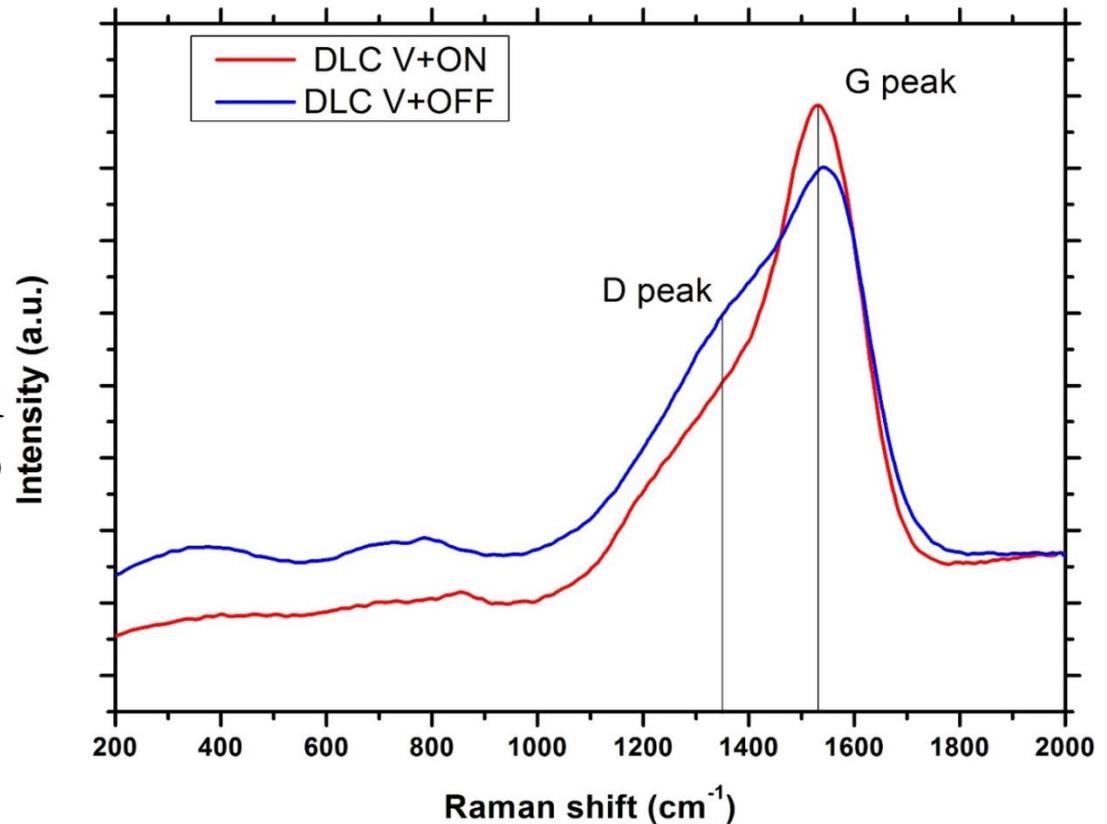


Effect of positive pulse reversal on the $sp^2:sp^3$ ratio of sputtered carbon

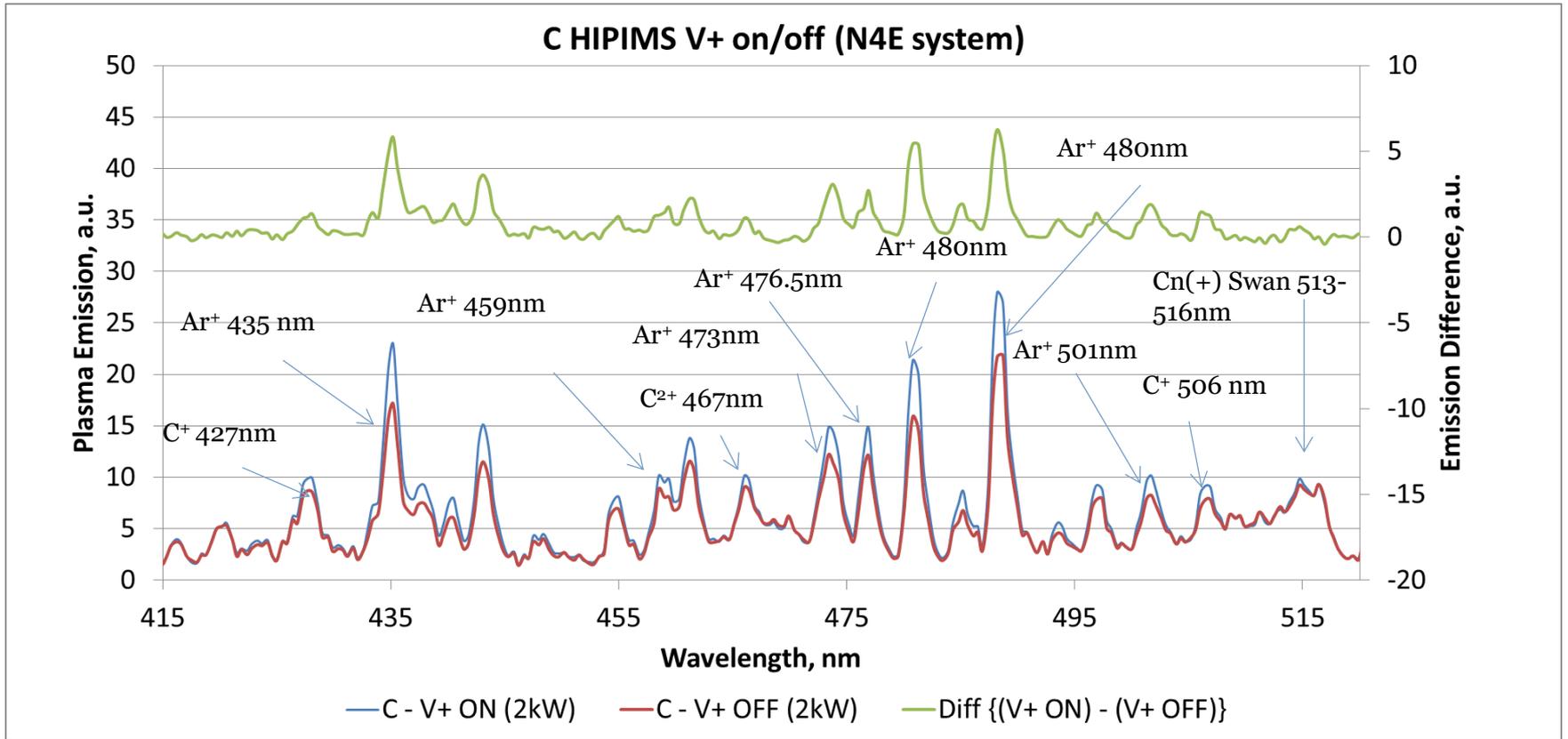
The positive pulse reversal and electron extraction creates an impact of positive ions onto the substrate

This increases the diamond sp^3 type bonding relative to the graphitic sp^2 bonding type

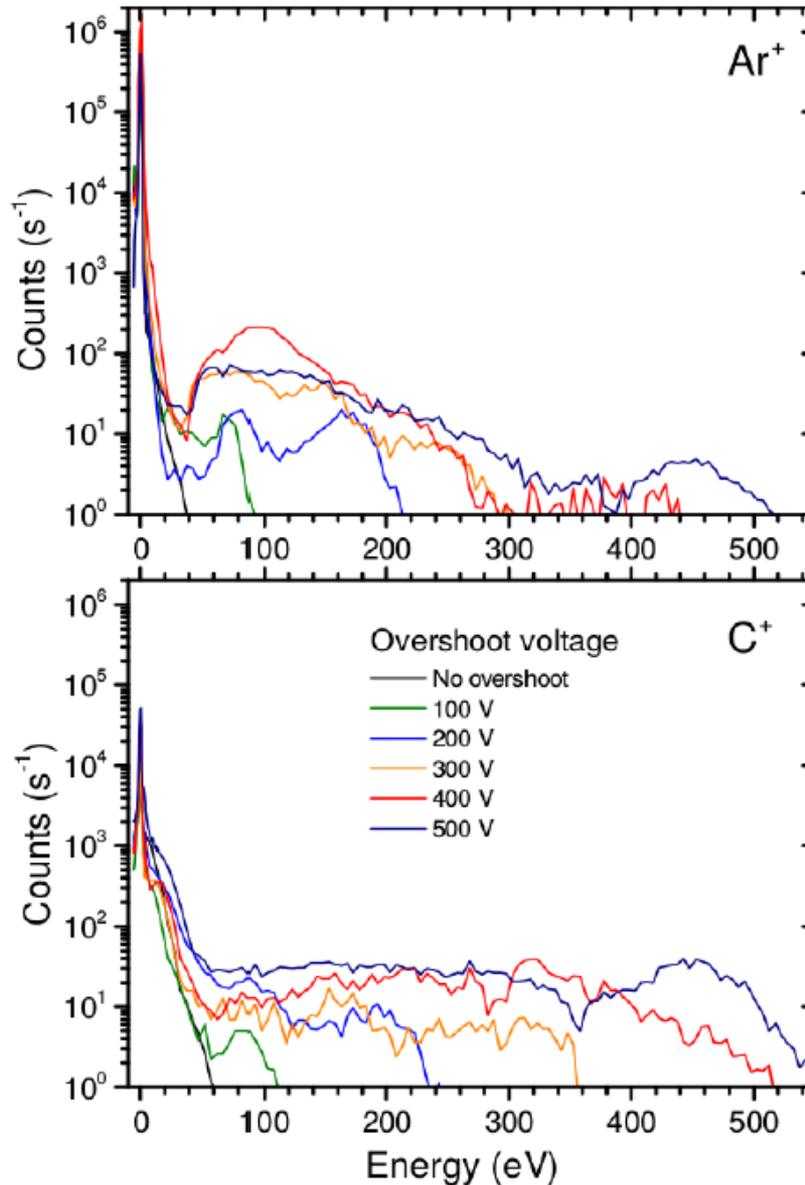
Higher levels of diamond type bonding increases hardness levels



The positive pulse reversal increases ionisation levels within the sputtering plasma as seen in the optical plasma emission spectrum below



Plasma mass spectrometry

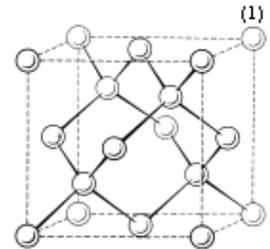
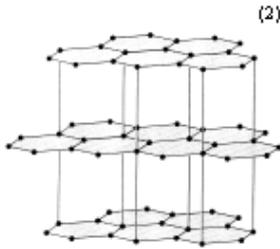
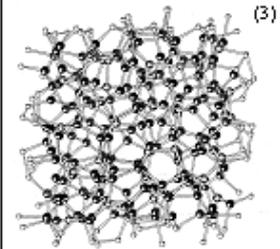


The positive overshoot is key to creating the ions needed to the bombardment of the growing film

The higher the positive overshoot the higher the energy of the ions that impact the growing layer

DLC on glass

Traditional bias not possible

Diamond films	Graphite	DLC
 <p>(1)</p>	 <p>(2)</p>	 <p>(3)</p>
C-C 100% sp^3 Crystal	C-C 100% sp^2 Crystal	C-C sp^3/sp^2 Amorphous

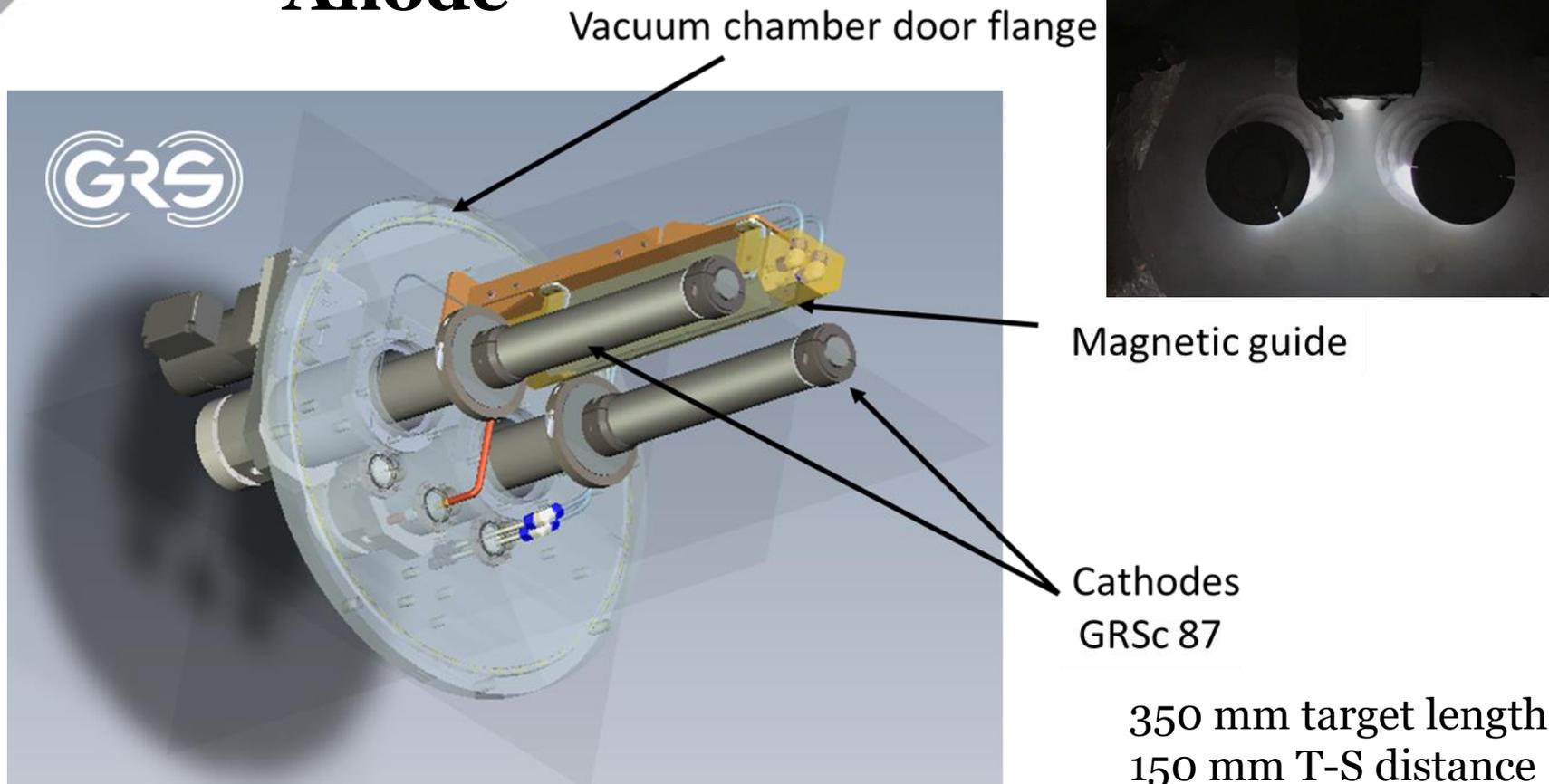


Typical bias on metal substrates enables hardness increase. Glass cannot easily be biased over a large area. The ion energy of impact dominates the hardness

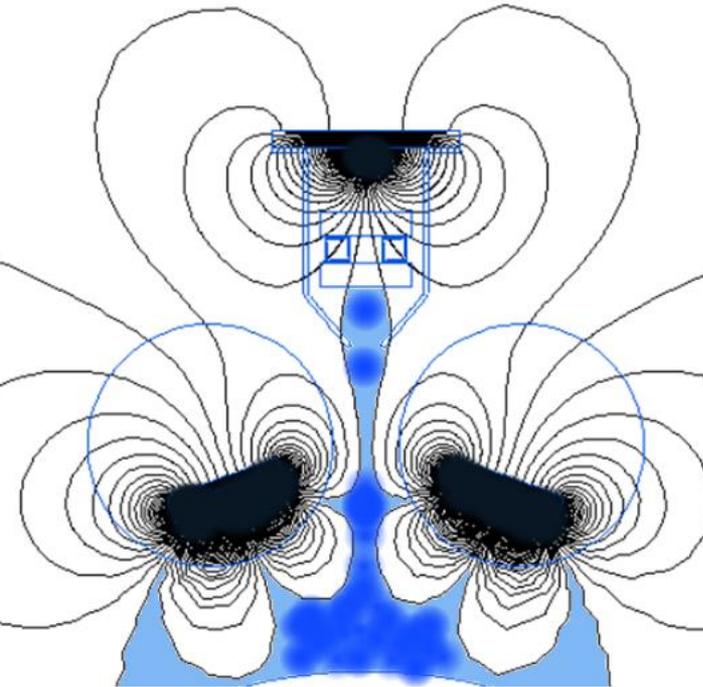
How to take advantage of this new method for abrasion resistant DLC on large area glass?

- Hipims discharges not practical for large area glass – current density too low for Hipims if target is much bigger than 1m in length.
- Rotatable magnetrons most suited to glass coating – carbon is a ‘dirty’ process, hence rotatables best.
- Switching AC or DC bipolar power modes standard in the large area glass industry.
- Hence work has been conducted based upon a dual rotatable with active anode and pulsed DC, AC and bipolar DC switching power to compare the benefits.

Experimental layout dual magnetron rotatable system – GRS C with Active Anode



Importance of electron extraction for hard DLC – Anode magnetic guidance

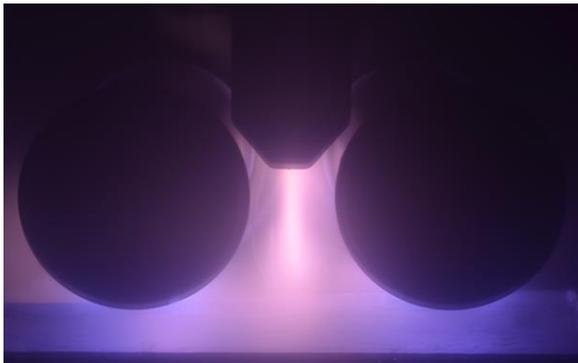


Gencoa patent for single or dual rotatables

• Improves coating density and lowers coating stress.

Essential for hard DLC on glass – otherwise graphitic.

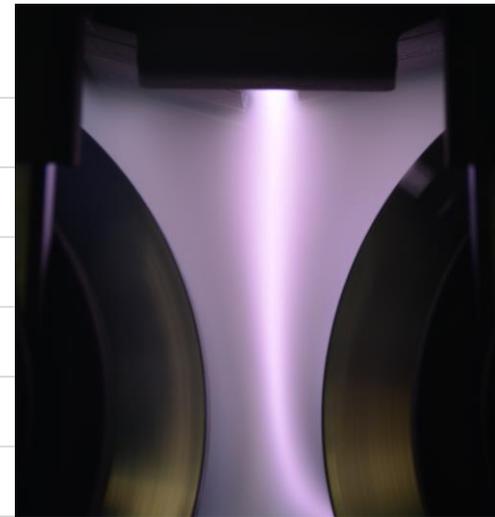
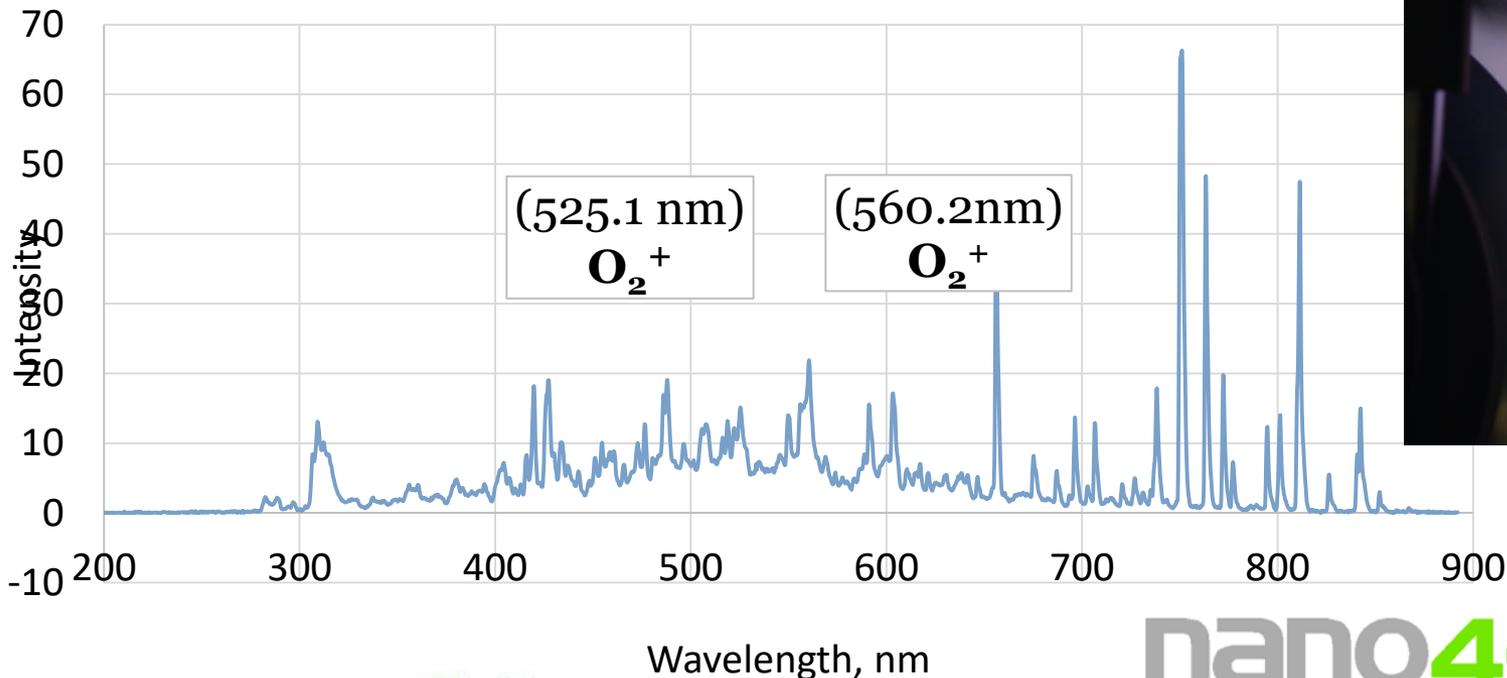
By using the magnetic field design of the magnetron and interaction with other magnetrons or magnetic active anodes, the electron current is separated from the ion current. This increases the impact of the ions and hardens the carbon layer & results in the doubling of the hardness.



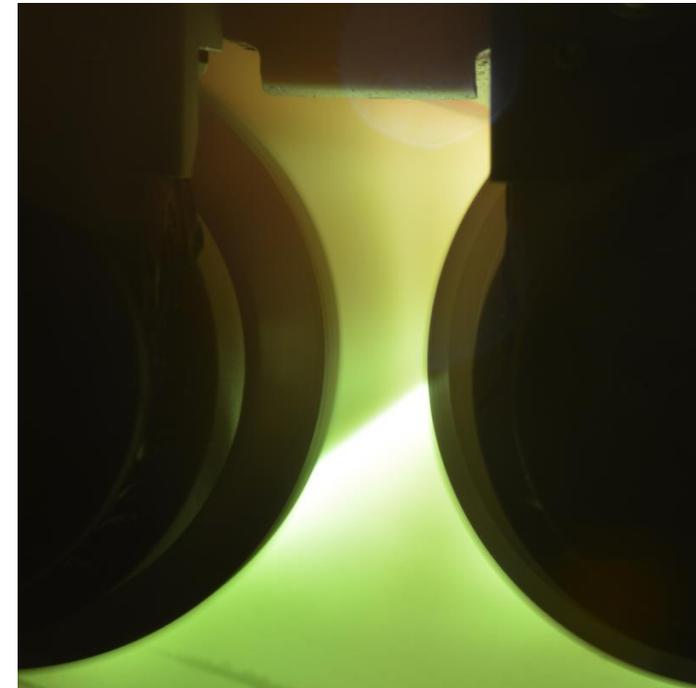
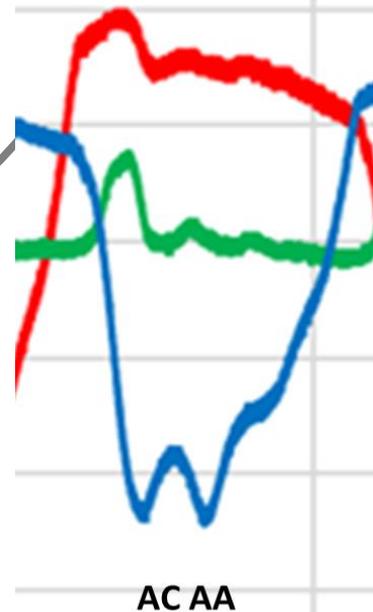
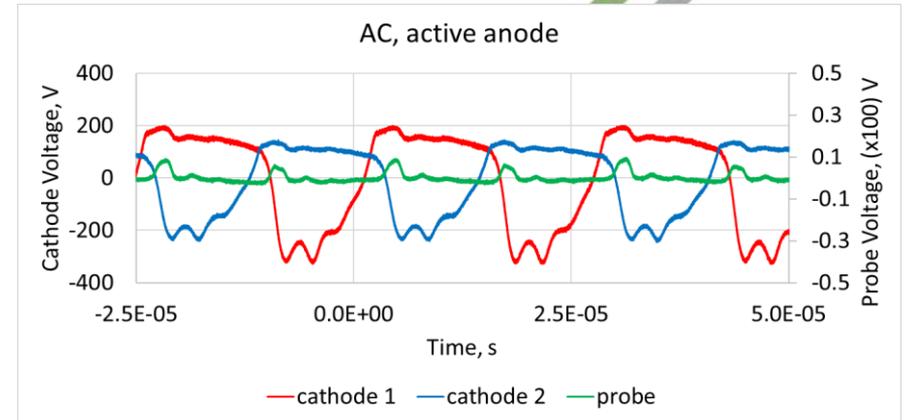
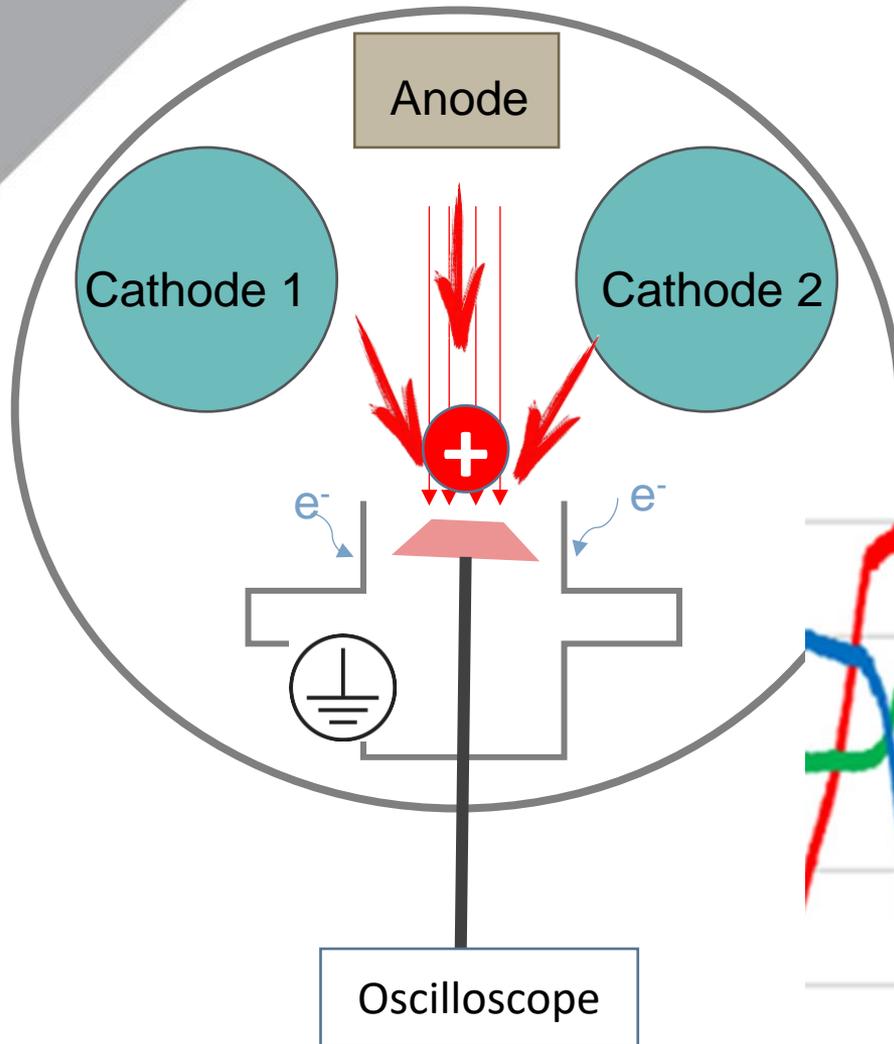
Introducing O_2 through the plasma in the anode zone increases the $V(+)$ pulse intensity and produces higher O_2^+ ionization

This method is used for pre-cleaning glass before DLC coating

Can be used for large area glass cleaning in general – 2 x carbon targets, AA and Ar/ O_2 gas mix with AC or switching power

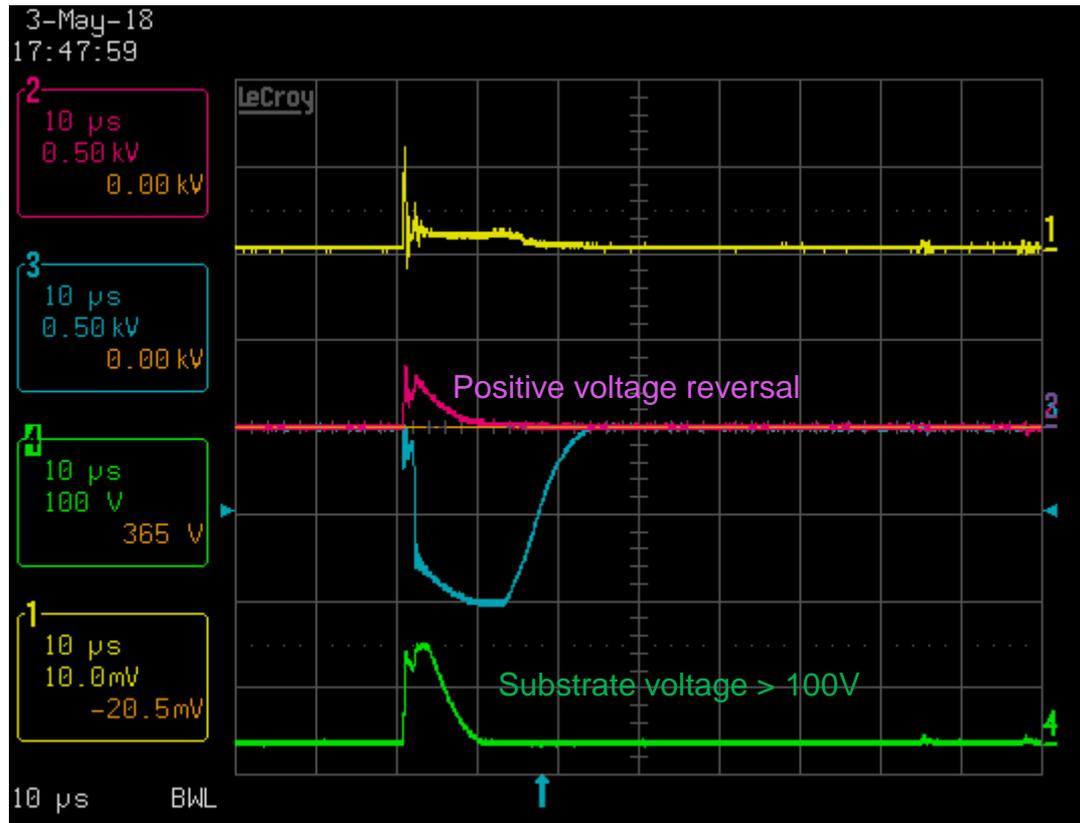


Active anode and AC power mode produces the positive Ar and O₂ bombardment



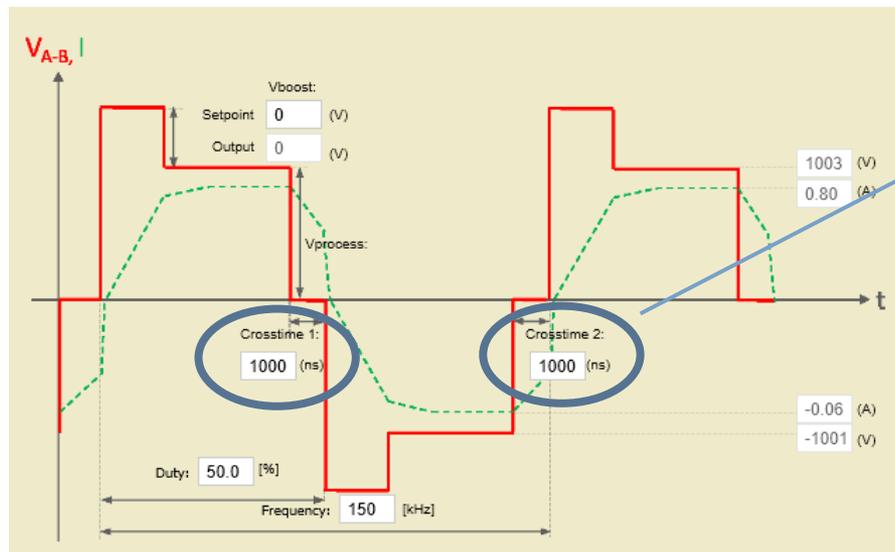
Dual rotatable GRSC & AA – with HIPIMS discharge – N₄E Power Supply

Cathode voltage reversal > 100 V biasing on the
substrate area



For large area glass AC or bipolar DC most suited - switching delays option

- A tweaked square-wave bipolar generator (AE Ascent DMS) is used for maximising a positive peak bias on the target surface, able to propel ions towards the sample

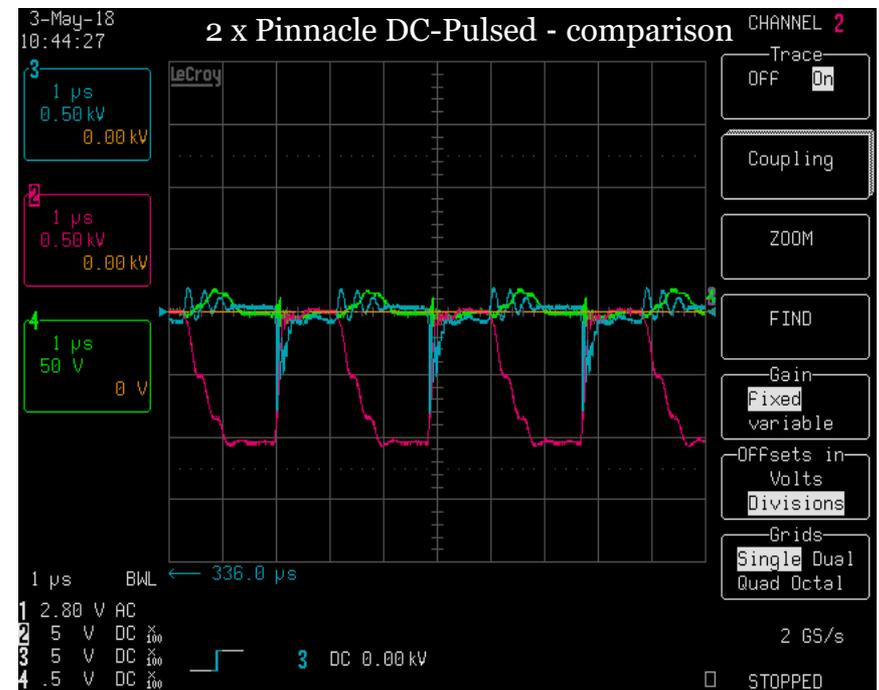
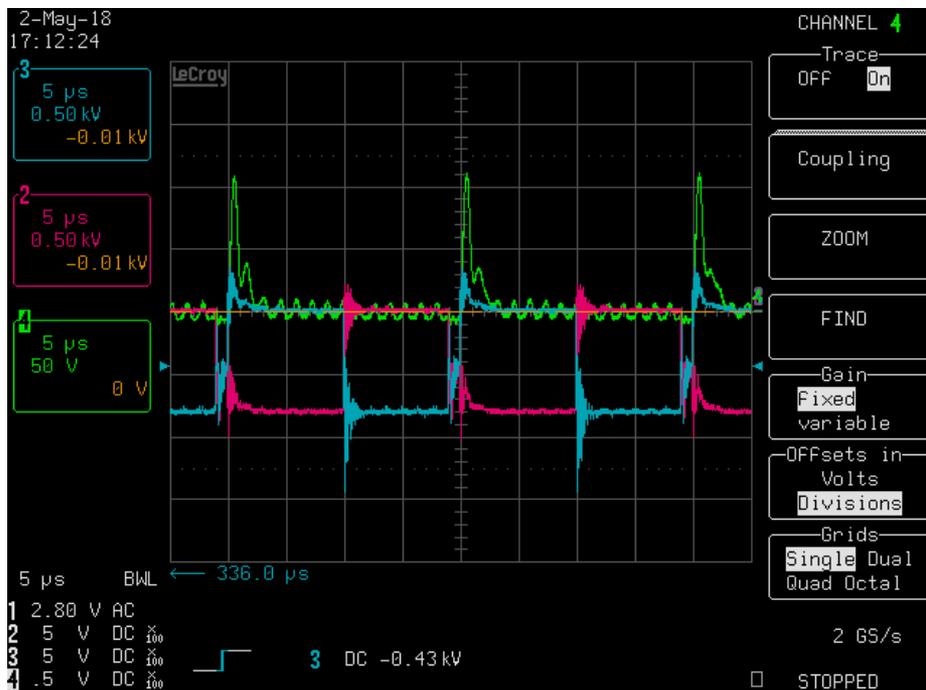


The cross-time or delay is the time off and can be set (max 1 μ s) within the duty cycle (max 2 delays per period)

During this time power is off. It affects the square-wave discharge inducing a sensibly higher peak-to-peak voltage

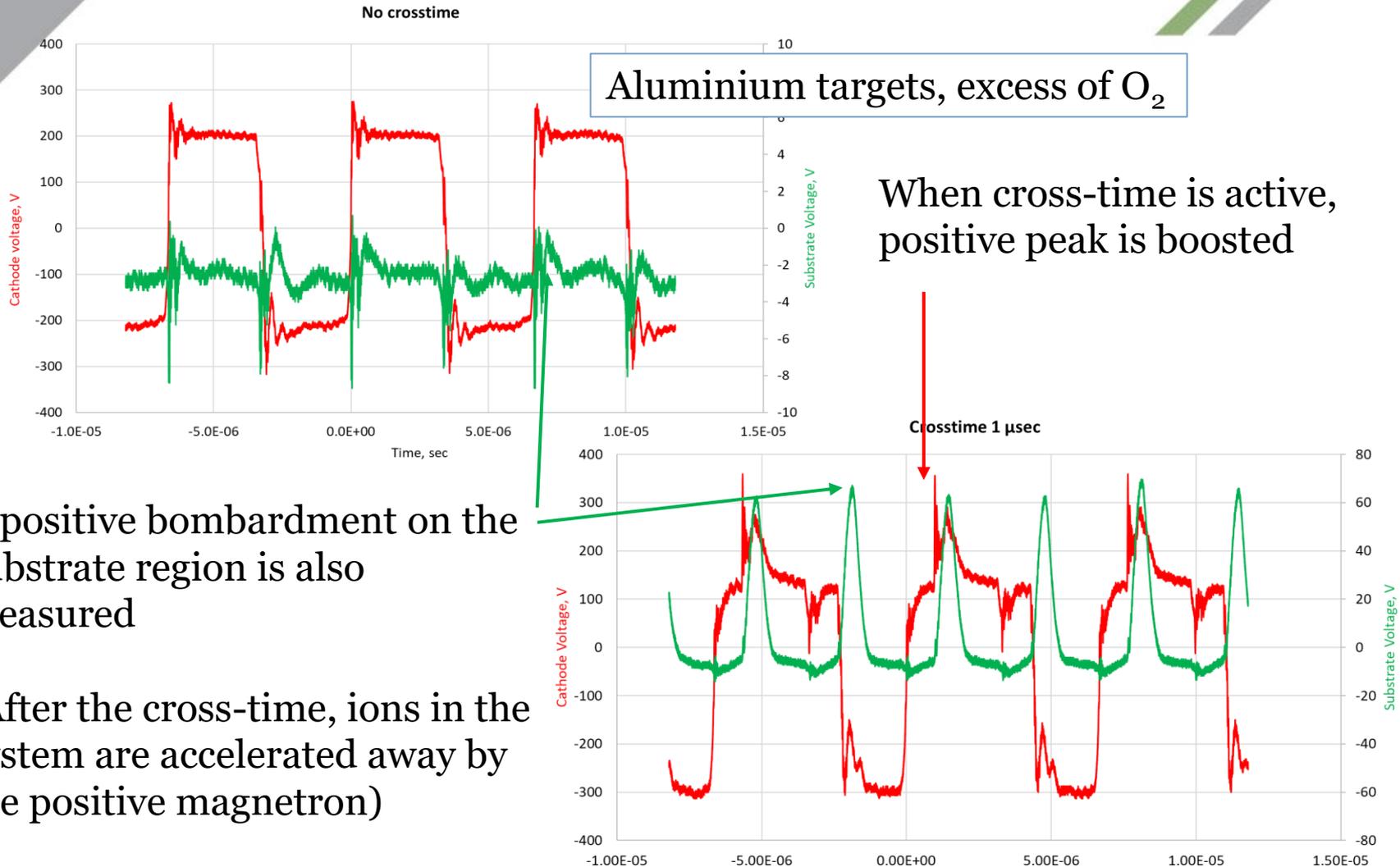
Dual bipolar discharge

Ion bombardment can be adjusted by inserting a delay after each cycle



Carbon targets

Positive bombardment with and without switching delay



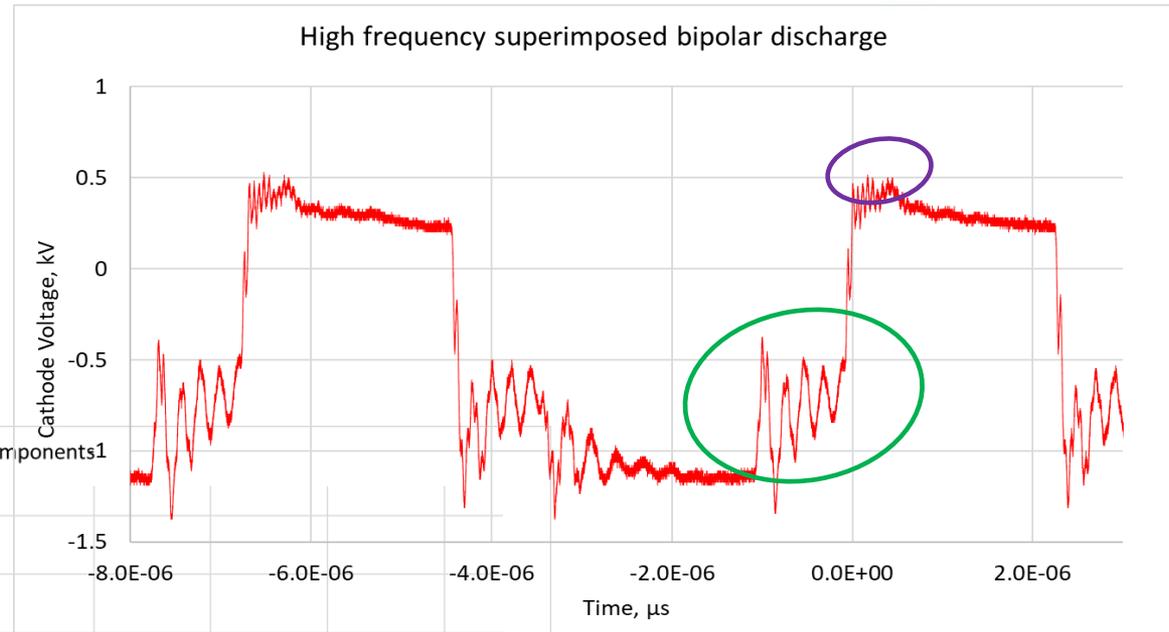
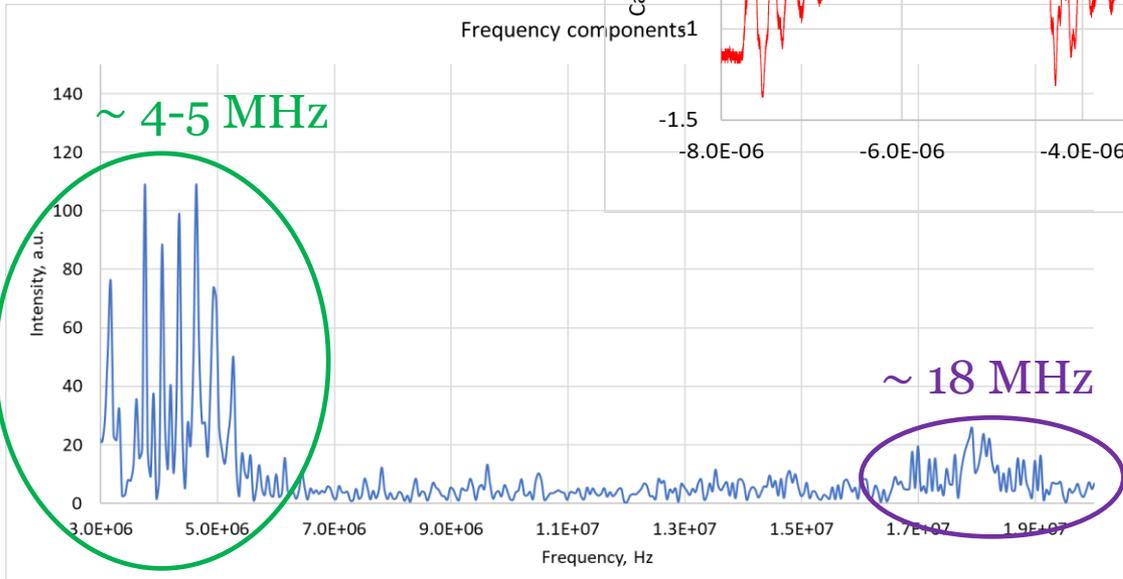
A positive bombardment on the substrate region is also measured

(After the cross-time, ions in the system are accelerated away by the positive magnetron)

Enhanced peak-to-peak voltage + high frequency discharge

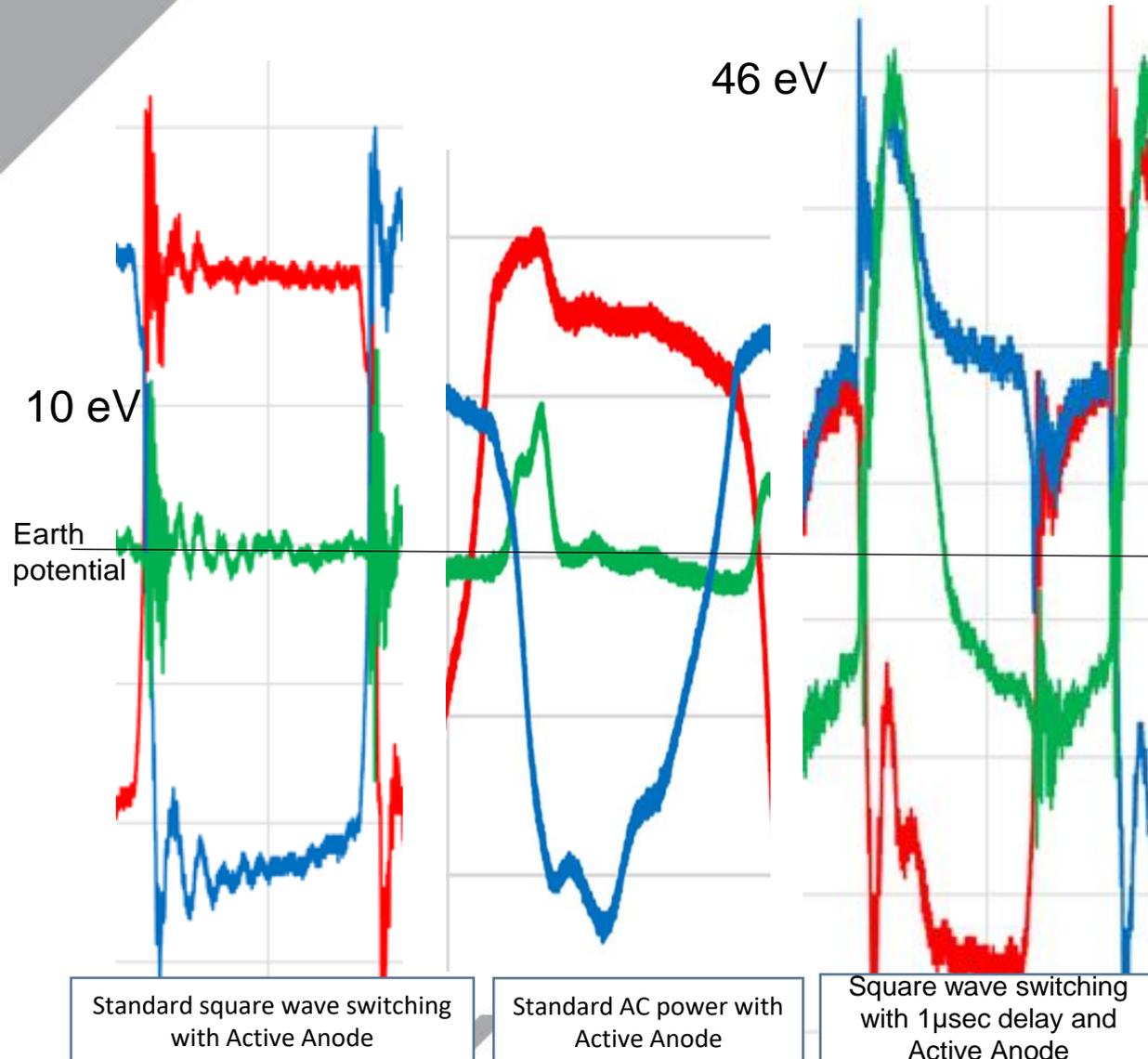
Main frequency is 150 kHz

DFT analysis of the discharge



High-frequency components are observed. These can play a role in ionisation enhancement

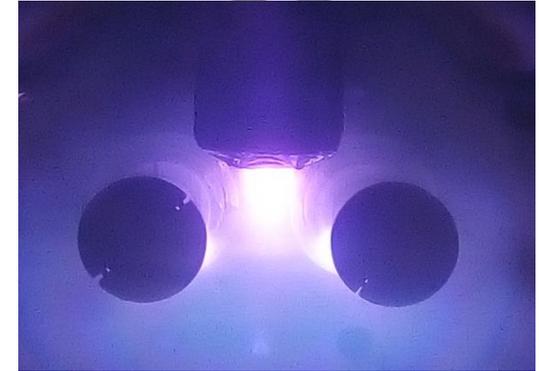
The Active Anode will create positive bombardment with all power modes – DC pulsed, AC, Hipims, DC Bipolar



- By switching electrons between targets extra ionisation is created
- Active Anodes AA creates positive and negative energy bursts on the substrate (ideal for glass or plastic substrates without external bias)
- Different levels depending upon power mode
- Introduction of a delay in the power switching increases positive energy

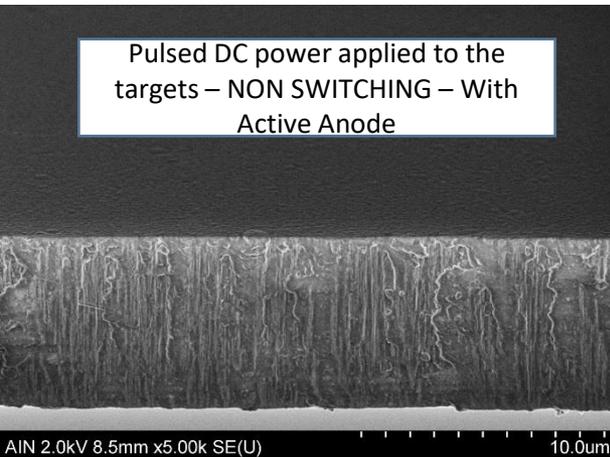
Creation of extra energy via power mode and Active Anode – comparison of coating structures

10 micron thick AlO_x deposited onto glass (floating potential – no external bias) from a dual rotatable magnetron and with active anode

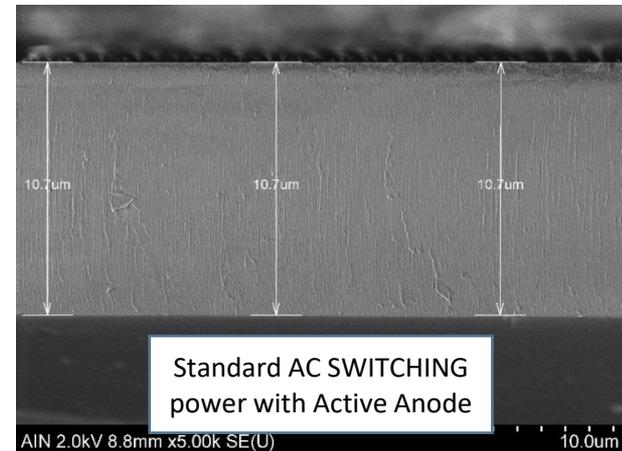
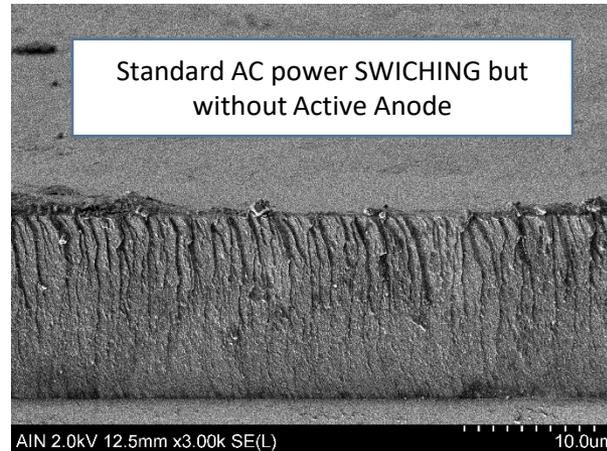


Increasing Energy Levels 

Pulsed DC power applied to the targets – NON SWITCHING – With Active Anode



Standard AC power SWITCHING but without Active Anode

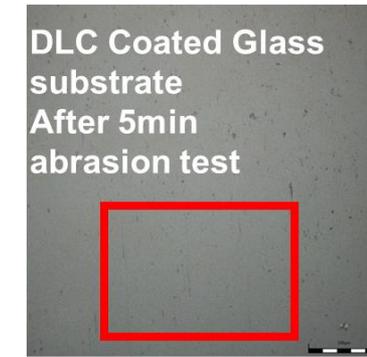
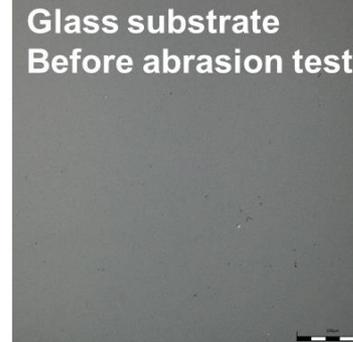
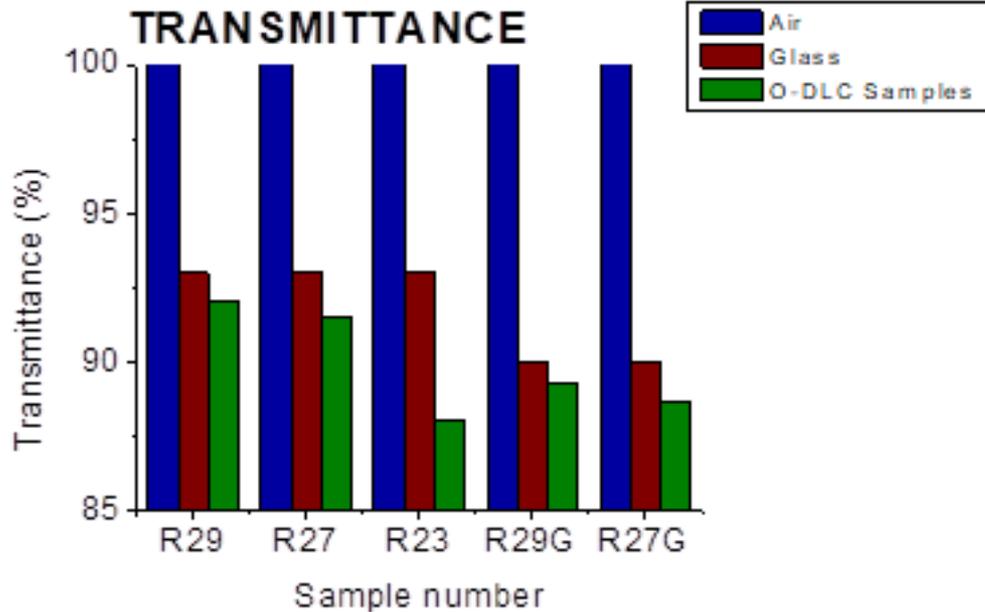


Columnar structures are recurrent when DC-Pulsed is used

AC switching power mode has improved structure compared to pulsed DC

AC with active anode Produces highly dense structure

DLC by this method is highly transparent – just 1% loss



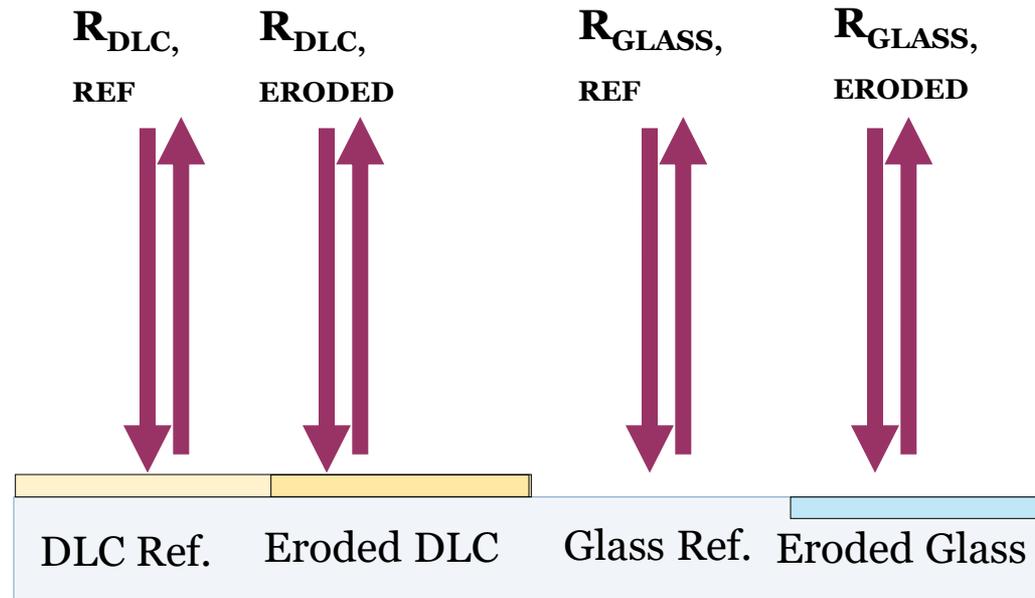
SAMPLE	Sample Transmittance (%)	Glass Transmittance (%)	$\Delta T_{DLC} = T_{glass} - T_{DLC}$ (%)
Air	100	-	-
R29 (10 nm)	92.0	93	1.0
R27 (15 nm)	91.5	93	1.5
R23 (125 nm)	88.0	93	5.0
R29G Thick glass(10 nm)	89.2	90	0.8
R27G Thick glass (15 nm)	88.6	90	1.4

2-5nm thick V±EE DLC on glass : Specular reflectance after abrasion tests

$$\Delta R_{\text{DLC}} = R_{\text{DLC, ERODED}} / R_{\text{DLC, REF}} \sim 5-10\%$$

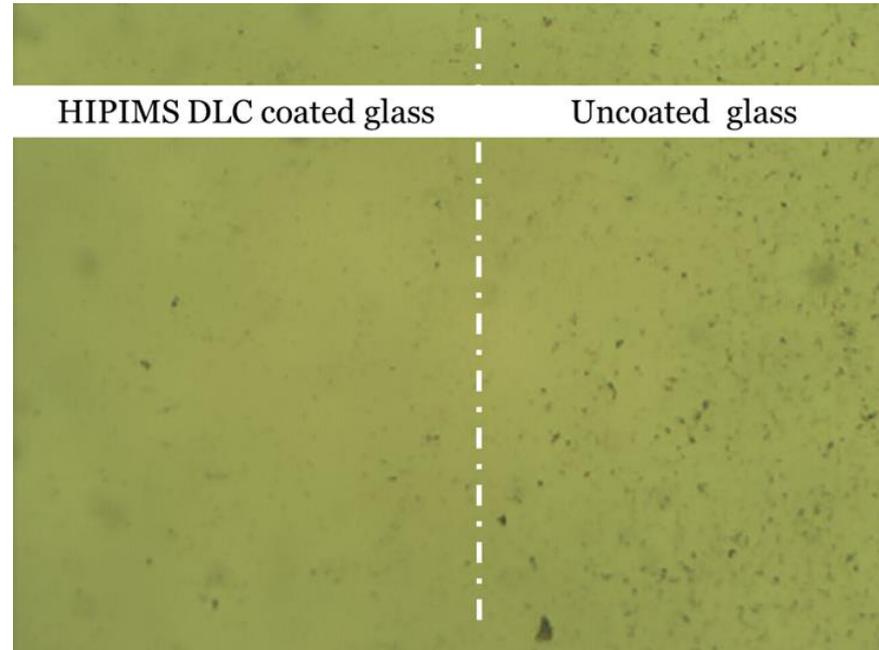
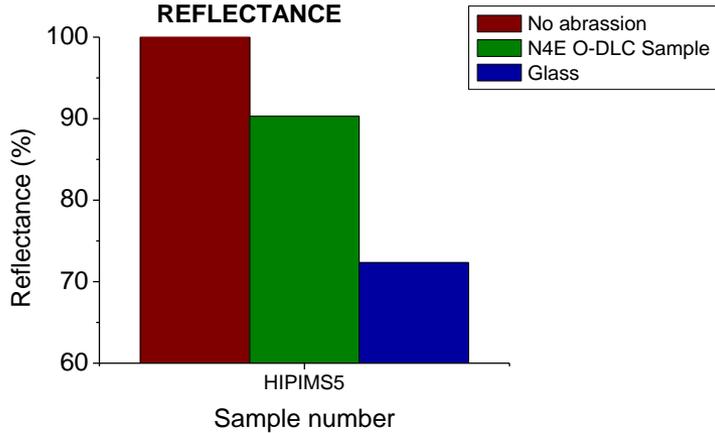
$$\Delta R_{\text{GLASS}} = R_{\text{GLASS, ERODED}} / R_{\text{GLASS, REF}} \sim 20-25\%$$

The samples are subject to 5 minutes sand oscillation test with silica sand



Abrasion tests DLC on glass

100x objective
Deuterium + halogen lamp
SpeedFlo CCD Spectrometer



After 5 min
abrasion test
x 10
magnification

SAMPLE	$R_{DLC, \text{ERODED}} / R_{DLC, \text{REF}}$ (%)	$R_{GLASS, \text{ERODED}} / R_{GLASS, \text{REF}}$ (%)	DLC Coating Improvement (%)
HIPIMS5 (5 nm)	90.3	72.3	18.0

* 5 minutes abrasion with “Sand oscillating test”
using Silica Sand

May 8th 2018

Optical DLC just 2 to 5nm thick provides scratch and abrasion resistance compared to uncoated

Sample Name	Thickness (nm)	Coating Transmittance (%)	$100 - \frac{R_{Coat,eroded}}{R_{coat,ref}}$ (%)	$100 - \frac{R_{Glass,eroded}}{R_{Glass,ref}}$ (%)	DLC Coating Improvement (%)
HIPIMS_5	5	87.2	9.7	27.7	18.0
HIPIMS_4	3.5	86.1	4.5	13.7	9.2
HIPIMS_6	2.8	86.3	1.4	7.8	6.4
HIPIMS_3	2.1	89.6	4.9	14.0	9.1
HIPIMS_7	3.5	90.3	3.3	15.3	12.0
HIPIMS_8	3.5	90.6	5.0	8.2	3.2
HIPIMS_9	3.5	90.8	2.9	19.0	16.1

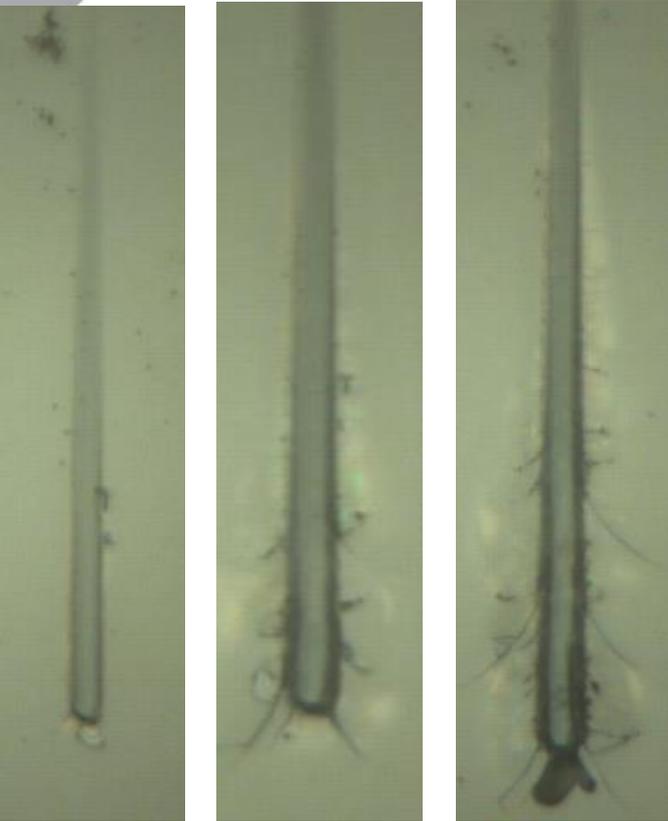
Microscratch tests on DLC coated glass

Conditions

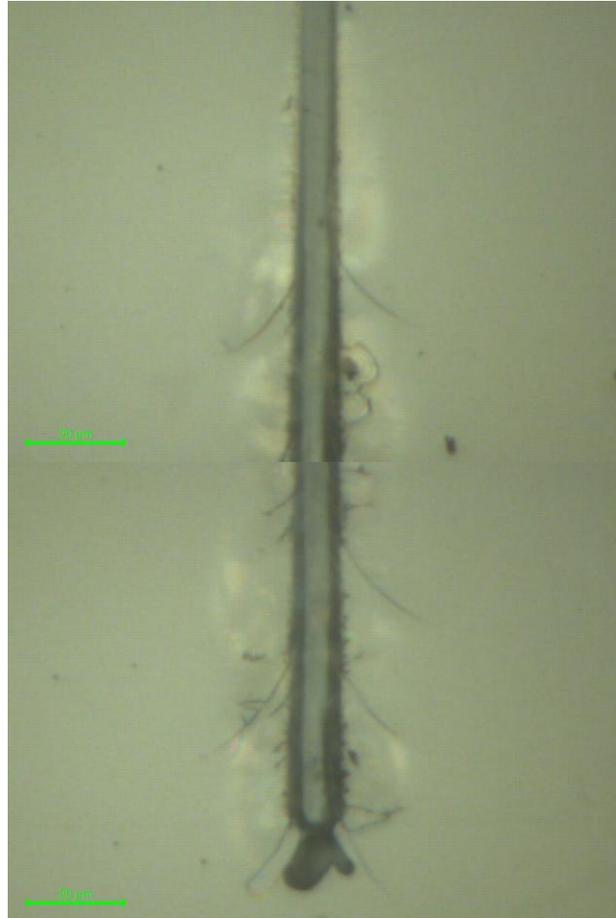
- Sphero-conical tip with a **tip radius** of 10 μm
- **Load rate** was 0.75 (mN/ μm) for thicker films (350nm) and it was reduced to 0.33 (mN/ μm) for under 100 nm films
- **Maximum normal load:** 500mN
- Scratch **length:** 300 μm
- 5 scratches in each sample
- All scratches were done at 1 mm away from one of the edges (to keep the rest of the sample clean for future experiments)
- Different **failure modes** for each sample

Microscratch tests on DLC coated glass

DLC_Cal_5



Scratch tracks (300, 400, 500 mN)



Critical load: ≈ 300 (mN)

Very good adhesion –
O₂ plasma pre-clean

Delamination failure

>8 Mohr hardness for
3nm thick DLC

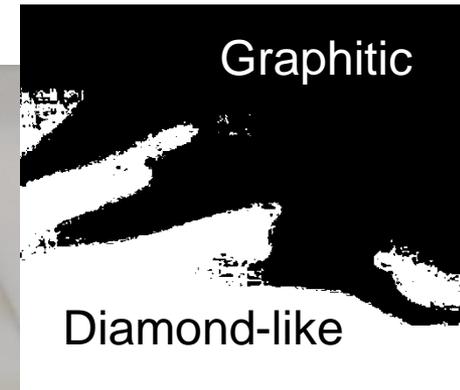
Temperature effect

If the glass is too hot, then graphitic rather than diamond like material will be deposited. Graphitic carbon, which appears darker, is thermodynamically more stable and is favoured at $> 150\text{ }^{\circ}\text{C}$.

The formation of DLC appears to occur when a good thermal contact between samples and metallic substrate holder is established.

The contact is casual in this case

The dark layer presents low-friction properties



Conclusions

- Hard, transparent and abrasion resistant DLC can be deposited on floating substrate as a result of combined positive voltage reversal on the target and electron extraction sputtering.
- This is achievable both with HIPIMS, AC, pulsed DC and dual bipolar power modes on planar or rotatable sources.
- The presence of a magnetic guidance of electrons away from the substrate is required for high ion bombardment.
- The hardware and power supplies are readily available to allow optical DLC on large area glass.
- The same arrangement can be used for plasma cleaning of glass via the use of Oxygen and carbon targets.
- The technology is already being used for the production of scratch resistant layers on glass.

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